

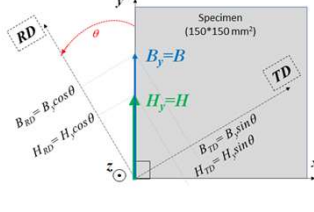
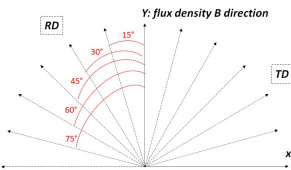
Investigating laser patterns for GOES submitted to misoriented flux with a 2D vector model.

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Introduction: Inductors and transformers with rectangular, U or E shaped magnetic cores have got corners or columns where the flux makes an angle with the Rolling Direction (RD). Any misoriented flux in a GOES significantly increases the losses by a factor from 2 to 5. This work contributes to the research on the ability of laser treatments to be locally compatible with misoriented flux inside electrical steels.

Samples & experiments

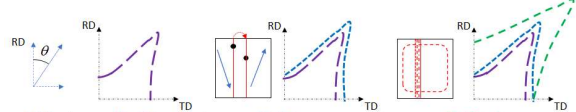
Standard conventional GOES SiFe grade R120-27 thickness = 0,27 mm



Samples cut with various angle v.s. RD
 Lis of samples defined below various laser patterns investigated for each

sample	ANGLE(Y, RD) / ANGLE(B, RD)	Direction of flux B measured and components in (TD, RD) frame
0	0=0°/0°	y (B _{TD} =B, B _{RD} =B=0)
0	0=0°/90°	x (B _{TD} =B=0, B _{RD} =B)
15	0=15°/15°	y (B _{TD} =B*cos15, B _{RD} =B*sin15)
15	0=15°/75°	x (B _{TD} =B*cos75, B _{RD} =B*sin75)
30	0=30°/30°	y (B _{TD} =B*cos30, B _{RD} =B*sin30)
30	0=30°/60°	x (B _{TD} =B*cos60, B _{RD} =B*sin60)
45	0=45°/45°	y (B _{TD} =B*cos45, B _{RD} =B*sin45)
45	0=45°/45°	x (B _{TD} =B*cos45, B _{RD} =B*sin45)
60	0=60°/60°	y (B _{TD} =B*cos60, B _{RD} =B*sin60)
60	0=60°/30°	x (B _{TD} =B*cos30, B _{RD} =B*sin30)
75	0=75°/75°	y (B _{TD} =B*cos75, B _{RD} =B*sin75)
75	0=75°/15°	x (B _{TD} =B*cos15, B _{RD} =B*sin15)
90	0=90°/90°	y (B _{TD} =B*cos90=0, B _{RD} =B*sin90=B)
90	0=90°/0°	x (B _{TD} =B*cos0=B, B _{RD} =B*sin0=0)

2D vector magnetic model



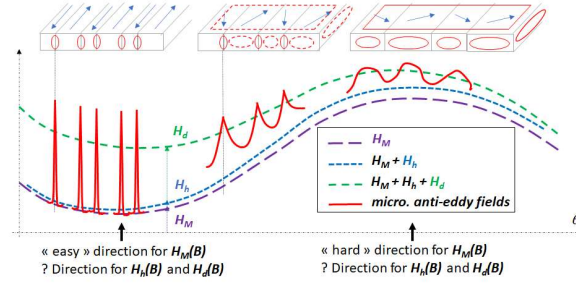
$$H(B, \omega) = H_M(B) + H_h(B) + H_d(B, \omega)$$

$$= [\mu_s(B)]^{-1} \cdot B + j[v_c(B)]B + j\omega \alpha [A]^2 \cdot B$$

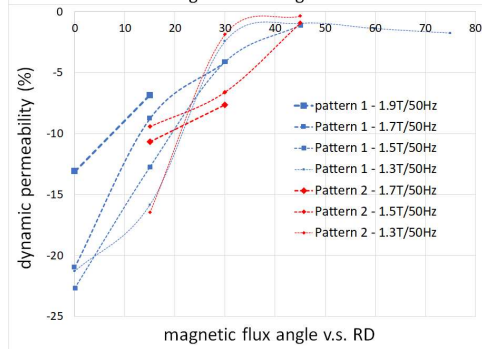
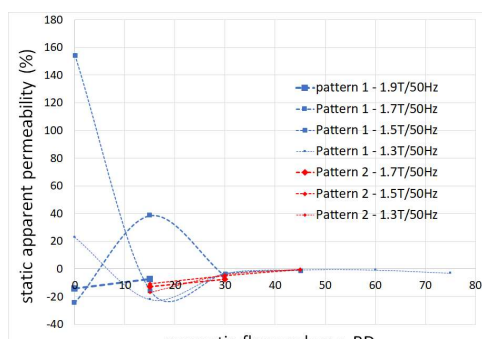
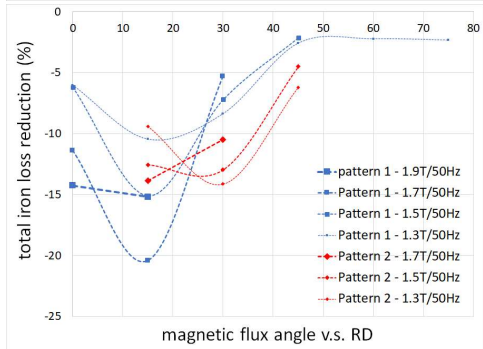
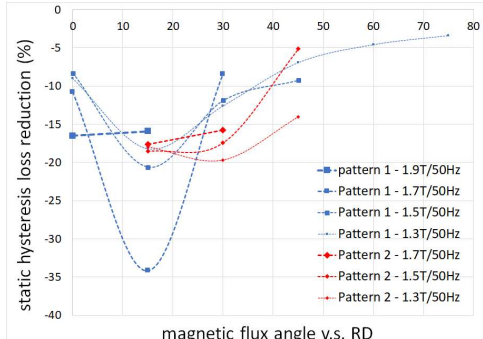
H_M: anhysteretic field from magnetic energy density e_M including magnetocrystalline, self and induced magnetic and shape anisotropy.
 $v_{c,mm} = -\frac{\partial e_M}{\partial B_m \partial B_n}$

H_h: coercive field from static hysteresis energy loss density e_h due to bowing and jumps of walls on the defects and grain boundaries.
 $v_{c,mm} = -\frac{\partial e_h}{\partial B_m \partial B_n}$

H_d: dynamic field from dynamic hysteresis energy loss density e_d i.e. microscopic eddy currents within nucleated magnetic domains and walls.
 $j\omega \sigma [\Lambda]_{mm}^2 = -\frac{\partial e_d}{\partial B_m \partial B_n}$



Results for a fundamental @ 50Hz v.s. angle between Flux direction and Rolling Direction (RD)



Conclusion: This ambition to control the loss reduction factors within misoriented flux requires to provide a vectorial description of the magnetic behaviour in 2D, able to predict the losses in any direction, and sensitive to the effect of a laser treatment in relationship with the magnetic domain structure.